

NOTICE OF EXPRESS MAILING

Express Mail Mailing Label Number: EL312581592US

Date of Deposit with USPS: April 12, 2000

Person making Deposit: Jared Turner

APPLICATION FOR LETTERS PATENT

for

**PROCESS FOR EXTRACTING QUANTITIES OF
PRECIOUS METALS**

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PROCESS FOR EXTRACTING QUANTITIES OF PRECIOUS METALS

BACKGROUND OF THE INVENTION

5 Field of the Invention: The present invention relates generally to the extraction of metals from materials. More specifically, the invention relates to the extraction of precious metals present in small quantities from particulate ore bodies, ore body derivative materials, residual industrial materials and the like.

10 State of the Art: The extraction of precious metals from ore bodies, ore body derivatives, or other materials containing trace quantities of precious metals is desirable where the extraction process is economically feasible and advantageous. Although precious metal rich materials are often targeted for precious metal recovery, millions of tons of material having trace amounts of precious metals are not processed using present methods of precious metal extraction for economic reasons. A economically feasible
15 process could convert the millions of tons of material having small or undetectable amounts of precious metals from virtually worthless material into a valuable commodity.

20 A number of processes exist by which precious metals are extracted from materials containing measurable quantities of desired precious metals. One of the processes involves the combination of a precious metal containing material with molten metal, such as lead, copper, iron, or a mixture thereof. The molten metal binds with the precious metals. The molten metal is separated from any extraneous material in the mixture, along with the bound precious metals, and the metal mixture is cooled. Known extraction and separation techniques may be used to separate the various metals from the cooled metal mixture.

25 Another process involves slurry cyaniding, wherein precious metals are extracted from metal using cyanide. However, the waste from such methods is harmful and is expensive to neutralize. Thus, such processes are not economically feasible where the precious metals contained in the material are apparent only in trace or undetectable amounts.

Other processes also exist, but none provide an economical method by which barely detectable or undetectable amounts of precious metals may be recovered from precious metal bearing materials. Therefore, an economical process providing for the recovery of precious metals from ore bodies, or waste materials which have only trace amounts of precious metals, is desirable.

BRIEF SUMMARY OF THE INVENTION

The present invention comprises a process for extracting metals from ore bodies, residual materials resulting from industrial processes and other materials containing small, or trace, quantities of one or more metals. Precious metals such as noble metals, platinum, palladium, gold, and silver are examples of the types of metals which may be recovered using the present invention. The process of the invention is particularly suitable for use in extraction of precious metals from materials to which application of conventional precious metal extraction processes is inefficient or prohibitively expensive. Such materials are referred to herein generically, for the sake of convenience, as "target materials".

The process of the present invention includes the steps of mixing a target material in particulate form with particulate metal, such as copper, and a material containing hydrocarbon chains, roasting the mixture, and recovering precious metals from the roasted mixture. One suitable material containing hydrocarbon chains comprises whole wheat flour. Roasting may include induction roasting in an induction furnace as well as roasting within a hydrogen furnace. The recovery of the precious metals from the roasted material is usually accomplished through smelting.

Mixing the target material with copper and, for example, flour involves the grinding of the target material to a desired particulate size, or mesh size, and the mixing together of substantially equal amounts of the target material, finely ground copper, and coarsely ground flour. The target material/copper/flour mixture is then passed to the roasting stage of the process.

During the roasting stage of the process, the mixture may undergo a single roast or a series of roasts before the final smelting process. Typically, one or more roasts are

conducted within induction furnaces operating at a high frequency such as, for example, about three thousand cycles per second (3kHz). The mixture is placed into a container, such as a crucible, which is inserted into an induction furnace operating at a temperature below the melting point of copper, or below approximately 2200 degrees F. The mixture ignites, usually immediately upon entering the induction furnace. Upon cessation of substantial burning of the mixture in the induction furnace, the mixture is removed and cooled in a substantially oxygen-free environment. A sealed container may be used to hold the cooling mixture. Carbon dioxide may be circulated through the sealed container to facilitate the cooling process and maintain the oxygen-free environment.

If more than one induction roast is performed, the previously roasted mixture is re-ground and combined with additional flour or other hydrocarbon chain containing material, the amounts of such material in this step being varied as required for optimal results. The roasting step is then repeated.

Optionally, a roasting step in a hydrogen enriched environment may be performed. Such a hydrogen roast involves the grinding of the target material followed by a roast in a hydrogen furnace rather than an induction furnace. The target material is placed in boats which facilitate hydrogen contact with the target material during the hydrogen roast.

Following the completion of the last roast, whether it is a hydrogen roast or an induction roast, the mixture is ground and mixed with about twice its weight in borax. The borax-post roast mixture is then smelted, for example in an induction furnace, to retrieve the precious metals from the target material mixture. The peak smelting temperature is preferably between about 3800 degrees F and 4000 degrees F.

BRIEF DESCRIPTION OF THE DRAWINGS

While the specification concludes with claims particularly pointing out and distinctly claiming that which is regarded as the present invention, the advantages of this invention can be more readily ascertained from the following description of the invention when read in conjunction with the accompanying drawings, in which:

FIG. 1 illustrates a general process flow diagram of the present invention;

FIG. 2 illustrates a specific flow diagram of the preparation stage of the process;
FIG. 3 illustrates a flow diagram of the first roasting stage of the present process;
FIG. 4 illustrates a container configuration to provide even heating of the target material;
FIG. 5 illustrates a container filled with a target material, having carbon rods inserted
5 therein, as an alternate method of injecting electromagnetic fields in a first roasting
 stage;
FIG. 6 illustrates a flow diagram of an optional hydrogen roast stage of the process; and
FIG. 7 illustrates a flow diagram of the smelting stage of the process.

10 DESCRIPTION OF THE ILLUSTRATED EMBODIMENTS

 A general process sequence of the present invention is illustrated in FIG. 1. Target
material 50 is passed to preparation stage 100. Prepared target material 55 is passed from
the preparation stage 100 to a first roasting stage 200 where the prepared target material
55 is induction roasted at least once and undergoes physical and chemical changes. Upon
15 completion of the first roasting stage 200, the induction-roasted target material 60 is
 passed to an optional second grinding and mixing operation. Following completion of the
second grinding and mixing operation, an optional second roast, stage 300, in the form of
a hydrocarbon roast further prepares target material 65 for a smelting process 400 where
noble metals such as platinum group, gold, and silver are collected from target material
20 65. Although FIG. 1 illustrates a process involving a single induction roast and a single
hydrogen roast, it is understood that other process sequences involving any combination
of induction roasts and hydrogen roasts also fall within the spirit of the present invention.

 Raw target material 50, for the purposes of defining this invention, refers to and
includes any ore body or derivative of an ore body, such as mine extractions, fly ash,
25 bottom ash from coal fired processes, mine tailings, coal ash, precipitants from various
leaching solutions (including by way of example only, HCl/Cl, Bromine, cyanide,
NaOH/KOH), pure elements, or any other material, such as a residual material from an
industrial process, which may, but not necessarily, contain at least trace amounts of one or
more precious metals. The inventive process is remarkable in its capability for extracting

precious metals from target materials 50 in which the presence of precious metal may be barely detectable, or even undetectable, by conventional assaying techniques. Thus, the inventive process may be applied to economically extract precious metals from target materials 50 which were heretofore considered to be waste, or of minimal value.

5 The extraction of precious metals from target material 50 involves a sequence of stages or process steps, and the extraction process of the present invention is hereinafter described with respect to a presently preferred embodiment for extracting precious metals from the target material.

10 The first stage of the process of the invention includes grinding and mixing of raw target material 50 into prepared target material 55. Conversion of the raw target material 50 to roasted target material 60 occurs in the roasting stage 200. FIG. 2 illustrates an exemplary flow diagram of the various steps in the preparation stage 100 to which the raw target material 50 is subjected to effect its conversion to prepared target material 55. The raw target material 50 entering the preparation stage 100 is fed into a grinder 110 where
15 the raw target material 50 is ground to a pre-determined particle size, preferably not larger than one hundred mesh. It has been found that a raw target material 50 particle size of one hundred mesh or smaller is desirable to ensure that each particle of target material 50 is subjected to a complete and thorough reaction in subsequent processing. Although a particle size of one hundred mesh is desirable, it is not, however, a critical limitation
20 because some effective conversion may take place with particle sizes larger than one hundred mesh.

25 Raw, particulate target material 50 from the grinder 110 is mixed with substantially equal portions, by weight, of copper 80 and flour 90. Thus, a one-to-one-to-one ratio of raw target material 50, copper 80 and flour 90 is combined and mixed in a mixer 120 to thoroughly mix the materials such that particles of each constituent are substantially in contact with particles of the other constituents. The mixture prepared in mixer 120 constitutes prepared target material 55, which is then fed to the first roasting 200 stage of the process. For example, if 227 grams of ground raw target material 50 are to be processed, it would be necessary to add 227 grams of copper 80 and 227 grams of flour

90 to the raw target material 50 and thoroughly mix the raw target material 50, copper 80 and flour 90 in the mixer 120. Although it has been found that a one-to-one-to-one ratio of raw target material 50, copper 80, and flour 90 is the preferred ratio, other ratios or combinations of these constituents may also effect some conversion and are considered within the scope of the present invention. Furthermore, a hydrocarbon material, rather than flour 90, may be substituted in the mixture of the prepared target material 55.

It is most preferable that the copper 80 combined with the raw target material 50 be almost pure, dendritic copper, or copper that is ground, or irregularly shaped. Copper 80 particles having a round or consistent shape are less desirable than irregular copper 80 particles having torn or jagged edges and surfaces, the latter providing enhanced surface area per unit weight for effecting greater conversion yield. Dendrite copper having a purity of about 999.0 to 999.9 is currently believed to provide the best yield of precious metals from the inventive extraction process. However, other purity values close to the desired purity may be used where copper 80 having a purity in a preferred range is unavailable. In addition to selecting an appropriate purity of the copper 80 used in the process, it is also necessary to select and employ an appropriate particle size of the copper 80. Particles of copper 80 having a mesh size of one hundred mesh or smaller are desired, and even finer particles are more desirable.

The flour 90 added to the raw target material 50 comprises flour 90 made from whole wheat. Although wheat in the form of flour is the preferred material, any suitable material containing hydrocarbon chains which may be broken with the application of heat and magnetic fields may be used. Plastics, other grains, and wood are examples of these kinds of materials, and may be referred to herein also as "hydrocarbon materials". Of course, if a material other than flour 90 is employed, the weight proportion of such other material may vary from that employed with flour 90. A coarse ground flour 90 is preferred over finely ground flour 90. Flour 90 providing a particle size distribution between about one hundred mesh to about twenty mesh fits this requirement.

FIG. 3 illustrates the components of the first roasting stage 200 of the process. The first roasting stage 200 begins with the transfer of the prepared target material 55

from the mixer 120 to one or more containers 210 these containers 210 are made of silicon carbide, which is a preferred material. Other containers 210 such as platinum, stainless steel, titanium, or other conductive material, which will withstand a minimum of 2500 degrees F, may be used and are within the spirit of the invention. However it has been shown that these other materials develop hot spots due to varying conductivity within the material or due to geometric placement with respect to the furnace coils in an induction furnace 220. Silicon carbide is much more forgiving as to these disadvantages, and is far cheaper than platinum. Containers 210 are used to hold the prepared target material 55 during an induction roasting process where the magnetic fields cause heat generation in the container walls, as well as penetrating through the target material 55. If a large quantity of prepared target material 55 requiring a container 210 with substantial volume is being processed at one time, a carbon rod 214 as shown in FIG. 4, or other conductive materials as previously mentioned, may be inserted into the prepared target material 55 within the container 210. Multiple carbon rods 214 may also be used as illustrated in FIG. 5. The placement of multiple carbon rods 214 as in FIG. 5 in the container 210 allows the formation of a conductive circuit which facilitates the heating of the target material 55. These methods are desirable to facilitate even temperature distribution throughout the prepared target material 55 during induction roasting. If a carbon rod 214, or any other materials capable of forming a conductive circuit, are used to ensure even heating throughout the prepared target material 55 they should be located and oriented to be no further than about eight inches from the side wall of the container 210.

As depicted in FIG. 3, prepared target material 55 is placed within a container 210 in an induction furnace 220 which is preheated to ignition temperature of the flour 90, then raised to just below the melting point of copper 80, or about 2200 degrees F. The prepared target material 55 within the container 210 ignites immediately due to the presence of the flour 90, producing a flame which is present throughout the roast. As the flour 90 in the prepared target material 55 burns, hydrogen gas is released from the breaking of hydrocarbon chains of the flour 90. The hydrogen gas reacts with the raw target material 50 and copper 80 comprising the remainder of prepared target material 55.

In addition, the burning of the prepared target material 55 forms carbon and carbon monoxide, both of which facilitate reduction of precious metals contained within the prepared target material 55 to a converted state. As combustible material is depleted from the prepared target material 55, the burning flame gradually subsides and the roasting of the prepared target material 55 is substantially complete when the flame is barely detectible. The flame commences as a blue, blue-green, or even yellow-blue-green color, and toward the end of the burn changes to a very light blue, being barely visually detectable. The roasted target material 60 is then removed from the induction furnace 220, and cooled in an oxygen depleted atmosphere. An exemplary roast time for 227 grams of raw target material 50 is about 45 minutes, with the roasted target material 60 being removed from the container 210 about 5 minutes before burning ceases. It should be noted, however, that the roast time will vary with the volume of material being roasted, a longer roast time being required for a larger volume.

An induction furnace 220 is used, in combination with the burning flour 90, to produce an oxygen-free and hydrogen rich environment for the roast of the prepared target material 55. Oxidation of the prepared target material 55 is undesirable because the materials are converted back to an oxide state which stops the conversion process of the invention and may even reverse it. A gas furnace should not be used in place of an induction furnace 220, as the former does not provide the required oxygen-free status, nor does it provide the desired frequencies of the changing magnetic fields.

Induction furnaces 220 used in the induction roasting stage 200 may be operated at a drive frequency between one thousand cycles per second (1kHz) and ten thousand cycles per second (10kHz), with a drive frequency of at least three thousand cycles per second (3kHz) being more preferred. Although there may be some conversion of prepared target material 55 at below three thousand cycles per second (3kHz), yields of precious metals when roasted within induction furnaces 220 operating outside of frequencies ranging upwardly from about three thousand cycles per second (3kHz) to about ten thousand cycles per second (10kHz) will be minimal. Optimized individual metal yields, including

those within the noble metals group, may be enhanced by selection of proper frequencies within the band mentioned above.

It is necessary that the temperature of the container 210 in the induction furnace 220 be maintained below the melting point of copper 80. If the temperature within the induction furnace 220 rises above the melting point of copper 80, the desired conversion in the prepared target material 55 does not occur due to the melting of copper 80. Therefore, the roast of the prepared target material 55 within the induction furnace 220 should be monitored closely.

Following the roast, the roasted target material 60 is cooled. Preferably, cooling of the roasted target material 60 is carried out in an oxygen-free environment. The roasted target material 60 is transferred from a container 210 to a sealed container 216 after substantially complete cessation of the burning of the flour 90. Substantially complete cessation of the burning of the flour 90 is evidenced by the lack of a discernable flame on or within the target material 55 within the induction furnace 220. The sealed container 216 may have at least one opening 217 for the introduction of carbon dioxide into the interior thereof. Introduction of carbon dioxide helps to prevent re-oxidation of the target material 60 while it is still hot.

Once the roasted target material 60 has cooled sufficiently, it is transferred to a grinder 230 where it is ground into particles having a size of one hundred mesh or smaller. The re-ground, roasted target material 60 may then be cycled through a second induction roasting process similar to the first roast. It has been found that a second induction roast may be advantageous for some target materials. Likewise, a third or subsequent series of induction roasts may also help increase the yield of precious metals in the final product, depending upon the constituency of the target material. However, it has been established that too many induction roasting steps may also drive the yield of precious metals toward a less precious metal such as silver, rather than, preferably, gold and platinum. It is also presently believed that a single induction roast, carried out at a frequency higher than three thousand cycles per second (3kHz), may provide a yield comparable to that of two roasts at a lower frequency.

target material 60 is transferred to a grinder 230 where it is reduced to particles having a mesh size of about one hundred or less. As noted above, a different grinder than grinder 110 is also preferred for this grinding process in order to prevent cross-contamination of material from different roasts.

5 Although not absolutely required for process function, it has been shown that yields of noble metals may be increased by roasting the target material 60 in a hydrogen atmosphere. When a hydrogen roast is added to the process, as shown in FIG. 6, stage 300, the roasted particulate (i.e. ground) target material 60 is transferred into boats 305 which are placed within the hydrogen furnace 310. The boats 305 are configured in such a
10 manner to allow the hydrogen in the hydrogen furnace 310 to permeate the roasted, particulate target material 60 in the boats. Typically, the boats 305 are of a material capable of withstanding temperatures in excess of 900 degrees C, such as stainless steel or graphite for example. The boats 305 are shaped to fit within the hydrogen furnace 310 and configured to allow hydrogen to permeate throughout the roasted target material 60
15 contained within the boats 305. Further, it is presently believed that the boats 305 should be filled to a depth not in excess of four (4) inches to facilitate such penetration. Of course, it is understood that the depth of the target material 60 in the boats 305, and the size of the boats 305, may vary with the capacity of the hydrogen furnace 310.

20 The preferred embodiment of the hydrogen furnace 310 is to surround the heating chamber with an induction coil to provide both heating and magnetic fields within the target material 60. The length of time to which the roasted target material 60 is exposed to the environment within the hydrogen furnace 310 varies depending upon the size of the boats 305 and the amount of roasted target material 60 being processed. It has been found that the hydrogen roast stage 300 is finished in about two hours at full temperature.
25 The amount of time required for the hydrogen roast may vary with the volume of material being roasted. The hydrogen furnace 310 is preferably a closed and contained furnace having a hydrogen atmosphere for the roast. An operating hydrogen furnace 310 temperature of about 850 to 900 degrees C is preferred, and about 900 degrees C is most preferred, during the hydrogen roast stage 300.

Following completion of any roasting processes, the number of which is determined by maximal conversion and whether the hydrogen roast stage 300 is used, the roasted target material, either 60 or 65, is ground in a grinder 230 or 330 respectively (depending upon whether a second induction roast has been conducted), to a particle size of one hundred mesh or smaller. The ground roasted target material 60 or 65 is mixed with borax 420 in a container 410 and smelted to recover the precious metals. The borax 420 may be in the form of borax powder or borax glass beads. Typically, the smelting 400 stage of the process involves the combination of the ground roasted target material 60 or 65 with about twice its weight in borax 420, erring on the side of excess borax 420, as depicted in FIG. 7. For example, 600 grams of roasted target material 60 or 65 may be mixed with about 1300 grams of borax 420. The mixture is then smelted to recover the precious metals. The smelting 400 stage is typically operated in an induction furnace 430 wherein the temperature is raised to a peak temperature of about 3800 degrees F to about 4000 degrees F, which has been found to be suitable for collecting gold, silver and platinum group metals within a copper matrix.

Smelting 400 is completed by pouring the molten metal 70 into bars, from which the precious metals, now in significant quantities and in substantially pure form, may be extracted by known processes, such as electrical-refining. Additional precious metal yields may be obtained by hydrogen roasting the slimes from the electrical-refining process with the same parameters previously mentioned for a hydrogen roast.

It has also been found that larger amounts of platinum group metals and gold may be obtained if an in-courting step is undertaken prior to smelting. In-courting is the addition of a small amount of precious metals to a mixture which is to be smelted. Typically, in-courting small amounts of the metals desired from the process tends to increase the amount of those metals actually recovered during the smelting process. For example, if prior to the smelting step 400, 1.5 grams of gold, 1.5 grams of platinum, 1.5 grams of paladium and 1.5 grams of silver are added to the ground roasted target material 60 or 65, the amounts of the respective precious metals recovered from the beginning 227

gram target material 50 may be improved by up to two times over the typical recovery achieved without in-courting.

Altitude has been shown to be a factor in performing the inventive process, in that higher altitudes decrease yield. A significantly decreased yield is experienced at an altitude of 2000 feet, decreasing steadily with increasing altitude.

The present invention involves the visible conversion of a target material containing substantially imperceptible quantities of precious metals into a material wherein such metals are clearly perceptible under a 200X microscope equipped with a good ring light. This conversion takes place during the series of roasts that may be applied.

The term conversion, as has been previously used in the description of the illustrated embodiments of this invention, is used to describe a probable low energy fusion process in which the nucleus of a light element fuses with the nucleus of another light element to form the nucleus of a heavier element. The reason for postulating this type of reaction is that careful analysis has shown no amounts, other than possibly trace amounts, of the noble metals present in the feed material to the process. After the process is complete careful analysis shows substantial amounts (some times running to thousands of ounces per ton) in the finished metal without adding any of the noble metals to any part of the process system.

The reaction vessel 210, such as is shown in FIG. 3 provides a complex environment that includes, but may not be limited to:

1. Heat generated through coupling energy from the furnace coil into the reaction vessel that becomes a shorted transformer turn;
2. Exposure of the contents of the reaction vessel to an intense varying magnetic fields at certain critical frequencies that are generated by the currents circulating in the furnace coils and in the walls of the reaction vessel; and
3. Opposing fields generated by currents traveling in both directions along the helical transmission lines formed by the furnace coil and penetrating the reaction vessel.

After formulating the well known equations governing electromagnetic fields, James Clerk Maxwell solved the equations with quaternians. This mathematical approach

resulted in forming field vectors that had not only magnitude and direction, but a scalar quantity representing potential as well. A simplified explanation of the significance of this approach is the example of two fields of equal magnitude but opposite direction interacting with each other. Using quaternions, the solution is a field with zero magnitude, no direction, and a scalar potential having a magnitude of two times the magnitude of the opposing fields. In an attempt to simplify the mathematical calculations used in electromagnetic field theory, Heaviside threw out the scalar results obtained with quaternions by reasoning that only the vector magnitudes and directions were of significance, thus greatly simplifying vector mathematics. This approach has become the method commonly used in electromagnetic field theory by science today. If we return to the original way Maxwell computed fields and consider the scalar quantities as localized metric potentials then it becomes possible to change the general space time metric within a localized space. It can be shown that nuclear binding forces, and therefore, nuclear reaction threshold, theoretically change if the space time metric changes. This may explain how it may be possible to provide a localized environment in which low energy nuclear fusion reactions could take place. A famous experiment in which chickens were fed only potassium yet continued to produce eggs with calcium shells indefinitely, shows that there are indeed low energy nuclear reactions in nature. One possible reaction of this type might be fusion of 5 Cu yielding $2 \text{ Au} + 45 \text{ H} + \text{two neutrons}$. This may occur in the present invention as there is a relatively large amount of carbon present near the end of the roast which would moderate the neutrons, thus providing slow neutrons for other reactions involving the lighter elements.

Having thus described certain preferred embodiments of the present invention, it is to be understood that the invention defined by the appended claims is not to be limited by particular details set forth in the above description, as many apparent variations thereof are possible without departing from the spirit or scope thereof as hereinafter claimed.